

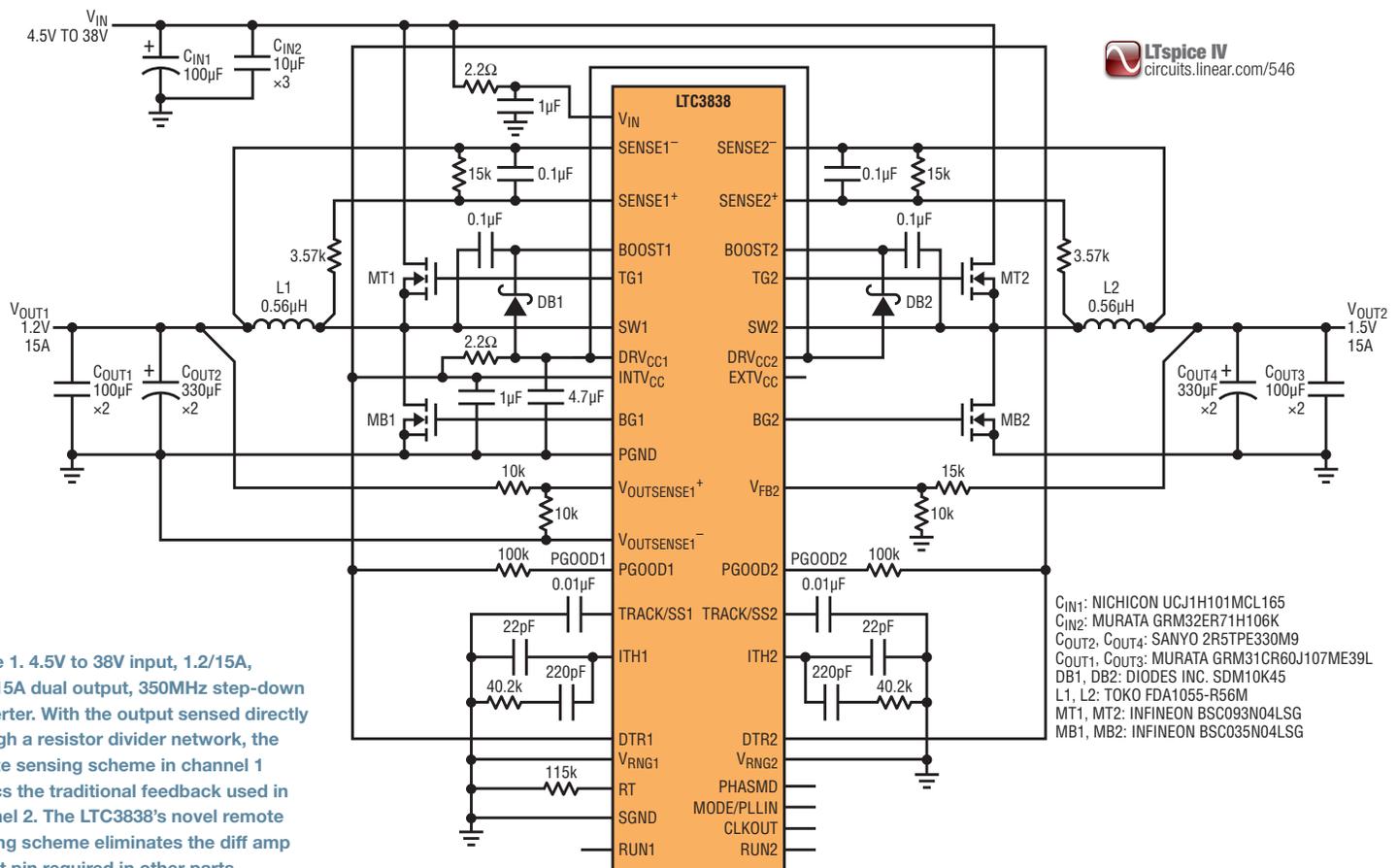
# 2MHz Dual DC/DC Controller Halves Settling Time of Load Release Transients, Features 0.67% Differential $V_{OUT}$ Accuracy and Is Primed for High Step-Down Ratios

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Electrical conditions once considered extreme are now the norm. Modern electronic systems demand high currents and very low voltages that can appear to a DC/DC converter as an intermittent electrical short. It is not uncommon for sub-0.9V power supply rails to demand 25A or more. In this environment, tight total differential regulation accuracy is critical to achieve the demanding voltage tolerances required to power core processors and large ASICs. In addition, PCB and component size constraints have driven up converter operating frequencies to enable the use of smaller components.

The LTC3838 and LTC3839 controllers are designed to meet the needs of the most demanding low output voltage, high load current applications. Both feature superior differential regulation accuracy and fast transient response. The controlled on-time architecture yields minimum on-times as low as 30ns and is capable of switching frequencies from 200kHz to 2MHz with synchronization to an external clock.

In addition to architectural advantages, the proprietary detect transient release (DTR) feature improves the transient



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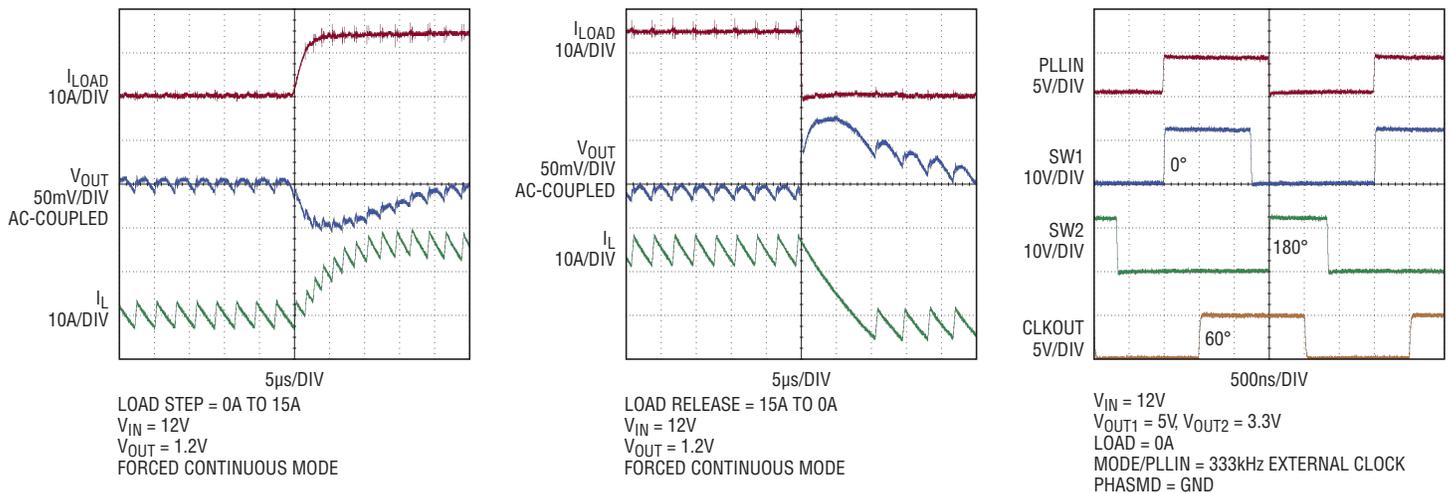


Figure 2. Switching frequency is constant and phase locked during steady state, but fast transient performance is achieved by momentarily adjusting the switching frequency: increasing it on a load step; decreasing it on a load release.

performance in high step-down ratio, low output voltage applications. This enables the LTC3838/LTC3839 to maintain accuracy and respond to load transients faster than other topologies.

In high output current supplies applications, it is important that *overall* regulation accuracy is well understood. To this end, the LTC3838 and LTC3839 internally combine the output differential amplifier and error amplifier and specify DC, line and load regulation output voltage errors as a single lumped parameter. This allows the LTC3838 and LTC3839 to achieve a level of total differential accuracy unavailable in other controllers.

The LTC3838 and LTC3839 make high frequency switching practical in a high input voltage, low output voltage converter. Both devices can produce high step-down ratios at high switching frequencies while maintaining high efficiency at heavy load

currents—previously challenging due to greater switching losses and limitations inherent in other architectures. For instance, in the typical 12V input to 3.3V/25A output application shown in Figure 3, the LTC3838/LTC3839 delivers a peak efficiency of 93% at 2MHz.

#### FLEXIBLE DUAL/SINGLE OUTPUT, HIGH ACCURACY REMOTE SENSE

The LTC3838's dual channels can be configured for either dual- or single-output applications, whereas the LTC3839 is dedicated for single-output applications. Both convert an input of 4.5V to 38V (40V abs max) down to outputs of 0.6V to 5.5V (6V abs max) in applications with per-channel currents up to 25A.

Their remotely sensed differential feedback has a voltage regulation accuracy of  $\pm 0.67\%$ —where the remote power ground can deviate as much as  $\pm 500mV$ .

The LTC3838's second channel can provide an independent  $\pm 1\%$  output, or together with the first channel, serve as one of the PolyPhase® channels for a single-output, higher current application. For higher load currents, or to maximize efficiency, multiple LTC3838s and LTC3839s can be paralleled for up to 12-phases.

#### FAST TRANSIENT PERFORMANCE, CONSTANT FREQUENCY

The LTC3838 and LTC3839 employ the new *controlled* on-time, valley current mode architecture, primed for fast transient performance. This architecture retains the benefits of a constant on-time controller: it responds to sudden load increases by a sequence of consecutive on-time pulses with a very short 90ns off-time in between, without having to wait until the next switching cycle like that of a fixed frequency controller. During a load release, the LTC3838/LTC3839 delays the turn-on of the top FET until inductor current drops

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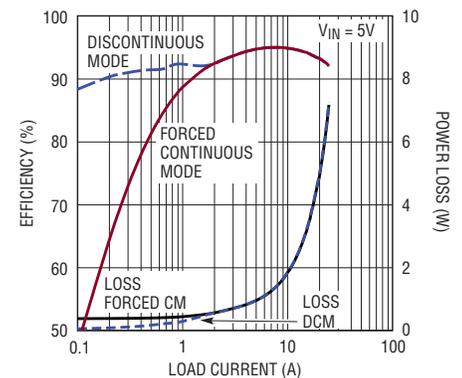
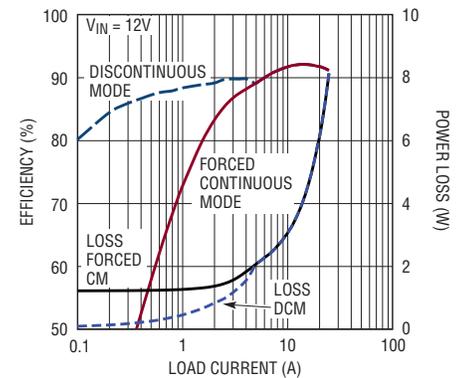
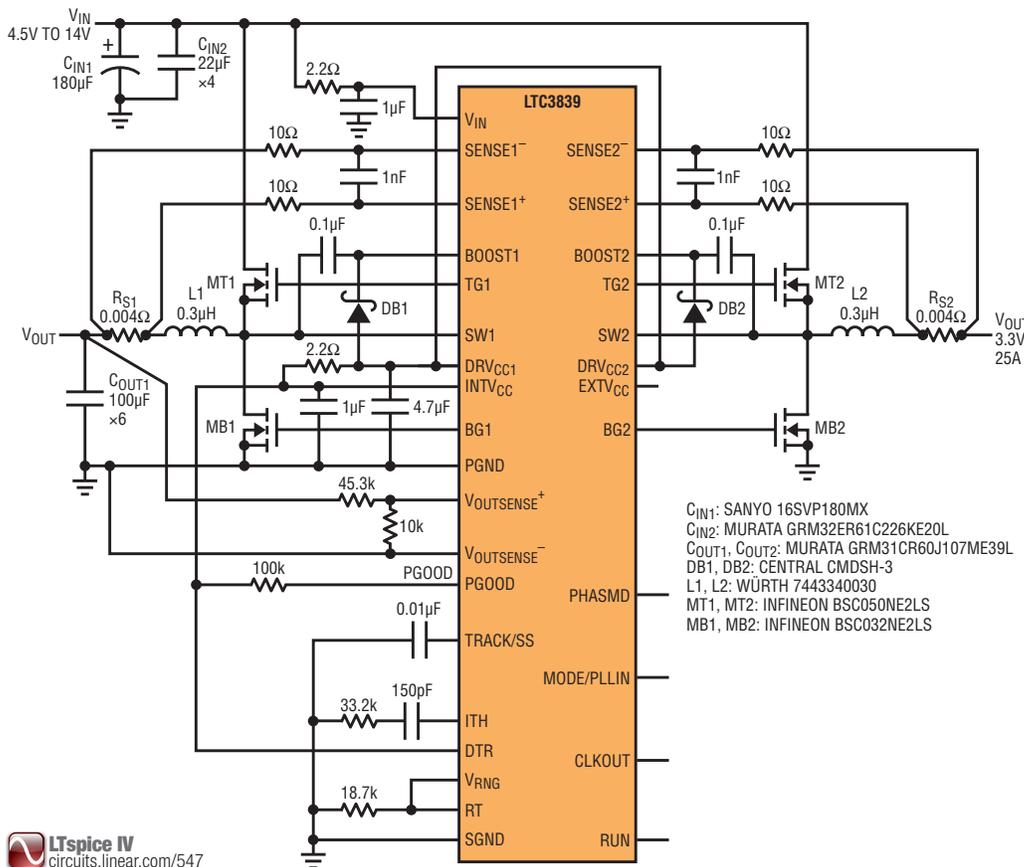


Figure 3. A 2MHz, 3.3V/25A step-down converter. The LTC3838/LTC3839 can operate at switching frequencies above the AM radio band ( $f_{sw} > 1.8\text{MHz}$ ). The high switching frequency permits the use of inductors of very small footprint, so that the entire circuit can fit within a  $0.9\text{in}^2$  area with both sides populated. The peak efficiency is 95%, and full load efficiency well above 90% at 25A, even at a frequency of 2MHz.

to desired value, preventing overcharging the output capacitor. Once the transient condition subsides, the switching frequency quickly returns to the programmed nominal or external clock frequency.

Meanwhile, the on-time is adjusted (hence *controlled* on-time) so that the switching frequency is constant during steady-state operation, synchronized to its internal programmable or an external

clock, to mimic a fixed frequency controller with predictable switching noise.

### HIGH AND WIDE STEP-DOWN RATIO, SWITCHING FREQUENCY

The LTC3838/LTC3839's 30ns minimum on-time (60ns effective on-time with dead-time delays) enables low duty cycles for high  $V_{IN}$  to low  $V_{OUT}$  applications, even while the part operates at high frequency. The 90ns minimum off-time

helps achieve high duty cycle operation and avoid output dropout when  $V_{IN}$  is only slightly above the regulated  $V_{OUT}$ .

The LTC3838 and LTC3839 are capable of a full decade programmable switching frequency from 200kHz to 2MHz. They can be synchronized to external clocks of  $\pm 30\%$  of the programmed frequency.



In addition to the LTC3838/LTC3839's architectural advantages, the proprietary detect transient release (DTR) feature improves the transient performance in low output voltage applications. This enables these parts to maintain accuracy and respond to load transients faster than other topologies.

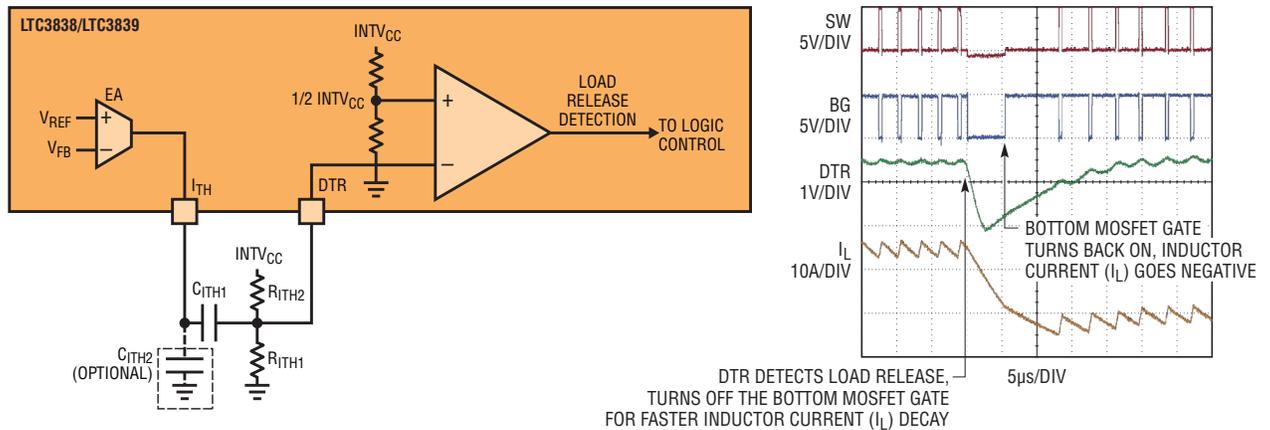


Figure 4. Transient detection is done through the detect-transient (DTR) pin, which is DC-biased slightly above  $\frac{1}{2} \text{INTV}_{\text{CC}}$ , and AC-coupled to  $\text{I}_{\text{TH}}$  pin through the compensation capacitor  $\text{C}_{\text{ITH1}}$ . The equivalent compensation resistance  $\text{R}_{\text{ITH}} = \text{R}_{\text{ITH1}} \parallel \text{R}_{\text{ITH2}}$ .

### NOVEL TRANSIENT DETECTION REDUCES LOAD-RELEASE $\text{V}_{\text{OUT}}$ OVERSHOOT

As the output voltage becomes lower and the  $\text{V}_{\text{IN-to-V}_{\text{OUT}}}$  step-down ratio increases, a major challenge is to limit the overshoot in  $\text{V}_{\text{OUT}}$  during a fast load current drop. An innovative feature of the LTC3838/LTC3839 is to detect “load-release” transients indirectly by monitoring the  $\text{I}_{\text{TH}}$  negative slew rate.

The detection is done through the detect-transient (DTR) pin that is coupled to  $\text{I}_{\text{TH}}$  pin through the compensation capacitor. At steady state, the DTR pin remains slightly higher than the detection threshold (half of the voltage on  $\text{INTV}_{\text{CC}}$  pin) with a voltage divider of the compensation resistors from  $\text{INTV}_{\text{CC}}$  to  $\text{SGND}$ .

In the event of a sudden drop of load current, the output voltage overshoots and  $\text{I}_{\text{TH}}$  slews down quickly. If the DTR pin drops below half of  $\text{INTV}_{\text{CC}}$ , the

LTC3838/LTC3839 temporarily turns off the bottom MOSFET, and the inductor current flows through the body diode of the bottom MOSFET. This increases the reverse voltage drop across the inductor, allowing the inductor current to drop to zero faster,

lowering the  $\text{V}_{\text{OUT}}$  overshoot by reducing overcharging of the output capacitor.

Once the inductor current reaches zero, the bottom MOSFET turns back on to pull the inductor current to negative, discharging the output capacitor to recover regulation.

Figure 5. Load-release detect transient (DTR) feature significantly reduces  $\text{V}_{\text{OUT}}$  overshoot and time to recover regulation. (Shades are obtained with infinite persistence on oscilloscope triggered at load release steps.)

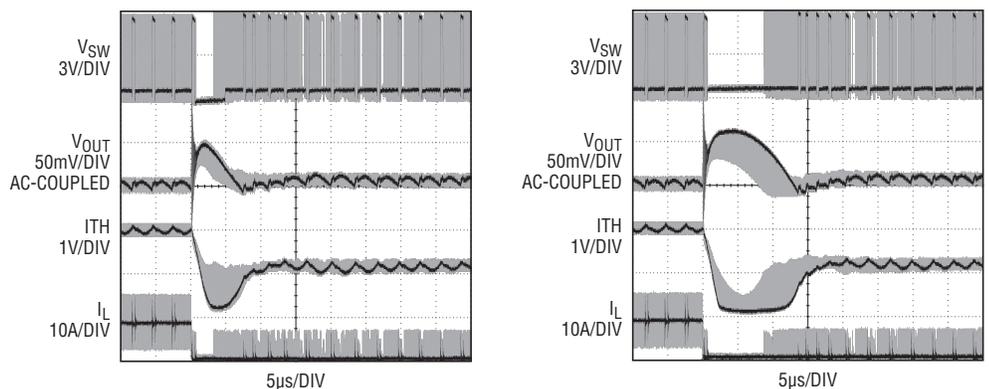


FIGURE 1 CIRCUIT, CHANNEL 1 MODIFIED:  
 •  $\text{R}_{\text{FB2}} = 0\Omega$ ,  $\text{V}_{\text{RNG2}} = \text{SGND}$ ,  $\text{C}_{\text{ITH1}} = 120\text{pF}$ ,  $\text{C}_{\text{ITH2}} = 0\text{pF}$ ,  
 • FROM DTR1 PIN:  $\text{R}_{\text{ITH1/2}} = 46.4\text{k}\Omega$  TO  $\text{SGND}$ ,  $42.2\text{k}\Omega$  TO  $\text{INTV}_{\text{CC}}$   
 $\text{V}_{\text{IN}} = 5\text{V}$ ,  $\text{LOAD RELEASE} = 15\text{A TO } 5\text{A}$ ,  $\text{V}_{\text{OUT}} = 0.6\text{V}$

- CONNECTION FROM  $\text{R}_{\text{ITH1/2}}$  AND  $\text{C}_{\text{ITH1}}$  TO DTR1 PIN REMOVED
- DTR1 PIN TIED TO  $\text{INTV}_{\text{CC}}$

